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the website about Vulcan Iron Works Inc. and the pile driving equipment it


## Critical Tension Stresses

G. G. Goble

When reinforced or prestressed concrete piles are driven in easy driving tension stresses are reflected from the pile tip back onto the downward traveling compression stresses. This can produce resultant tension stresses in the pile that can be sufficiently large enough to cause tension cracking of the concrete. This problem can be analyzed by use of a "Wave Equation" analysis. If measurements are made they are usually made with transducers located near the pile top. However, the critical tension stress location will not be at the gage location so the magnitude of maximum tension stresses cannot be readily determined. In this paper a procedure will be presented for determining the maximum tension stress in the pile given measurements at the pile top. In addition a procedure will be discussed for calculating maximum tension stress using a closed form solution of a continuous model of the pile.

Because excessive tension stresses are most likely to occur during easy driving, at times when the soil resistance is small in comparison to the maximum hammer force delivered, one can make a rough approximation of the time and location of the maximum tension stress by consideration of the hammer force wave alone. In Figure 1, hammer force pulse, idealized for clarity, is shown in various stages of propagation. While the shape of this wave is not realistic, it embodies the important characteristics of observed hammer-induced waves: A rapid rise time to the force peak and a gradual decay with time of the force. The time from impact to the maximum force is denoted by $t_{p}$. The ends of the rod are considered to be
free, and a wave is reflected from a free end as a force wave of the same shape but opposite sign. Hence, upon encountering the pile toe, the compression wave from the hammer is reflected in tension. The stress at any section after $t=L / C$, as shown in Figure $1 b$, is given by the difference between the upward traveling tension wave and the downward traveling compression wave (the so-called tail). The maximum tension force will occur when the difference between these two is the greatest. However, to complicate matters, when the hammer wave returns to the pile top, it is reflected a second time from a free end, and becomes compression again. So, the location of the maximum tension stress is as shown in Figure 1 c , a distance of $t_{p} / 2$ from the pile top, where $c$ is the speed of wave propagation in the pile. This depth will be referred to as $x_{c}$, the critical section. The compression force induced in the pile at the critical section and time ( $x_{c}, t=2 L / c+t_{p} / 2$ ) serves to reduce the maximum force by superposition. Examination of Figure lc shows that this force is $F(2 L / C)$, where $F$, as defined above, is the input force at the pile top. This force value will be denoted by $F_{t}$, the so-called "tail" force. Close consideration will reveal that the use of a more realistic force wave will yield the same results.

Now consider a more realistic case where top measurements are available as shown in Fig. 2. The force and velocity measurements at the pile top are shown. The force in the reflection wave is related to the measured force and velocity at a time $2 L / c$ after impact, the time necessary for the original impact wave to travel the length of the pile, reflect and return to the measuring location. If we define

$$
\phi=V(E A / C)-F
$$



Fipure 1. Reterminetion of Critical Location
at time $2 L / c$ then the force in the tension reflection $T_{R}$ is $\phi / 2$.
As shown in Fig. 2, the tension force at any location $x$ (which occurs at a time ( $2 L-x) / \mathrm{c}$ after impact) is the sum of the reflected tension force and the input wave measured at time $2 x / c$ before $2 L / c$. If the input wave exceeds the tension reflection force $T_{R}$, then no net . tension exists. This approach can be used for all locations along the pile so that a tension envelope, $T(x)$, is obtained and from it the maximum tension. The tension envelope is given by superposition with the velocity input wave. Thus,

$$
T(x)=\phi / 2-(E A / c) \vee(\{2 L-2 x\} / c) \geq 0
$$



Figure 2. Maximum Tension Example

The concepts used above can be used to obtain a direct solution to the problem without the necessity of a "Wave Equation" computer analysis. Referring again to Figure 1 it can be seen that to solve the problem $F_{\text {max }}$ and $t_{p}$ must be known together with the shape of the "tail" of the curve. In addition the reduction of the reflected tension by tip resistances must. also be known. This problem was solved by Parker (Reference) for air/steam hammers using a model shown in Figure 3. By writing the equations of motion of the masses and imposing a boundary condition relating the cushion spring force and the pile top velocity two third order differential equations are obtained. The solution can be of two forms.

$$
\begin{gathered}
F(t)=V_{h} e^{-2 t}(A \cos w t+B \sin w t) \\
F(t)=V_{h}\left(P e^{-s_{1} t}+Q e^{-S_{2} t}\right)
\end{gathered}
$$



Figure 3. Pile Model by Parker

The constants $\alpha, \omega, A, B, S, S_{2}, P, Q$ are complicated in their definition. Therefore, they have been tabulated for a variety of typical values of driving system parameters.

In application this method is used by obtaining the values for $F_{\max }$ and $t_{p}$ from the tables in the Appendix. If $t_{p}$ is known the location of the critical tension stress is known and therefore the associated time for calculating the force coming into the pile in the "tail" of the curve.

The method will be illustrated by a numerical example. The following nine-step procedure can be used to estiamte the maximum tension stress in a pile.

Step 1 Establish Driving System Constants Weights of Ram and Helmet ( $R$ and $H$ ) in Kips Stiffness of Capblock and Cushion ( $K$ and $C$ ) in Kips/Inch

$$
\begin{aligned}
V_{h} & =\text { Hammer Impact Velocity }(\mathrm{ft} / \mathrm{sec}) \\
& =\sqrt{2 \mathrm{gh(eff)}}
\end{aligned}
$$

where

$$
\begin{aligned}
g & =\text { Acceleration of Gravity }\left(\mathrm{ft} / \mathrm{sec}^{2}\right) \\
h & =\text { Stroke (ft) } \\
\text { eff } & =\text { Hammer Efficiency } \\
c & =\text { Wave Speed } \\
& =\frac{\text { Eg }}{\gamma}
\end{aligned}
$$

where

$$
\begin{aligned}
& \left.E=\text { Young's Modulus (kips/ft }{ }^{2}\right) \\
& y=\text { Weight Density of Pile (kips/cu ft) }
\end{aligned}
$$

NOTE: Convert $c$ to $\mathrm{ft} / \mathrm{Msec}$ for use with method

Step 2 Find Force Pulse Constants from the Appendix
Step 3 Find Critical Depth

$$
x_{c}=c t_{p} / 2
$$

Step 4 Find Maximum Force Delivered by Hammer

$$
F_{\max }=(F / V) V_{h}
$$

Step 5 Find $F_{t}$, Hammer Force at Time Delay $2 \mathrm{~L} / \mathrm{c}$
$t_{d}=2 L / c$
TYPE I Solution

$$
F_{t}=V_{h} e^{-\alpha t_{d}}\left\{A \cos \left(\omega t_{d}\right)+B \sin \left(\omega t_{d}\right)\right\}
$$

TYPE II Solution

$$
F_{t}=V_{h}\left\{P e^{-s_{1} t_{d}}+Q e^{-s_{2} t} d\right\}
$$

Step $6 \quad$ Find $F_{s}$, Effect of Soil Resistance at Critical Section Use Table 1

Step 7 Find $F_{d}$, Effect of Soil Damping
$F_{d}=2 J_{c} F_{\max }$

Step 8 Find Maximum Tension Force, $T_{\text {max }}$
$T_{\text {max }}=F_{\text {max }}-F_{t}-F_{s}-F_{d}$
Step $9 \quad$ Find Maximum Tension Stress
$\sigma_{t}=\frac{T \max }{A}$

EXAMPLE
Situation
An 80-foot long, 20 -inch square $H C$ pile has a prestress of 1.0 ksi . A Vulcan 020 Hammer has been chosen to assure that this pile can attain its
highest ultimate capacity. To reach a sufficiently strong stratum, the piles must first pierce a thin, hard layer overlaying softer material. The geotechnical consultant predicts that this layer will exert a side force of 40 tons on the pile during driving and recommends a Case damping constant of $J_{C}=0.1$.

Problem
Select a cushion made of $3 / 4$-inch plywood sheets to prevent pile breakage.

Solution
Try a cushion of three sheets of $3 / 4$-inch plywood.
Step 1 Establish Driving System Constants
Hammer: $R=20.0 \mathrm{kips}$
Stroke $=36$ inches

$$
\begin{aligned}
V_{h} & =\sqrt{2 \mathrm{gh}(\mathrm{eff})} \quad \text { (Assume } 80 \% \text { efficiency) } \\
& =12.4 \mathrm{ft} / \mathrm{sec}
\end{aligned}
$$

Helmet: $H=2.2$ kips

$$
K=60000 . \mathrm{kips} / \mathrm{inc}
$$

Cushion: $\quad C=\frac{A E}{L}$

$$
A=400 \mathrm{in}^{2} \text { (Pile top area) }
$$

$$
E=30.0 \mathrm{ksi} \text { (Assumed for plywood) }
$$

$$
L=3\left(3 / 4^{\prime \prime}\right)(p .75) \quad(25 \% \text { shortening assumed })
$$

$$
C=7100 \mathrm{k} / \mathrm{in}
$$

Wave Speed: $\quad c=\frac{E g}{\gamma}$

$$
\begin{aligned}
& =\quad \frac{(4000}{\times 144)(32.2)} \\
& =11,120 \mathrm{ft} / \mathrm{sec}=11.12 \mathrm{ft} / \mathrm{Msec}
\end{aligned}
$$

Step 2
$C=6000$
$\alpha=0.291$
$\omega=0.071$
$A=-12.6$
$B=737.2$

$$
C=8000
$$

$$
s_{1}=0.547
$$

$$
s_{2}=0.217
$$

$$
P=-202
$$

$$
Q=215
$$

$$
C=7100
$$

$$
t_{p}=2.8
$$

$$
F / V=73.2
$$

Step 3 Find Critical Depth

$$
\begin{aligned}
x_{c} & =c t_{p} / 2 \\
& =11.12(2.8) / 2 \\
& =15.6 \mathrm{ft}
\end{aligned}
$$

Step 4 Find $F_{\max }$

$$
\begin{aligned}
F_{\max } & =(F / V) V_{h} \\
& =(73.2) 12.4 \\
& =908 \mathrm{kips}
\end{aligned}
$$

r
Step 5 Find $\mathrm{F}_{\mathrm{t}}$
$t_{d}=\frac{2 L}{c}=\frac{2(80)}{11.12}=14.4 \mathrm{Msec}$
TYPE I Solution $\quad(C=6000)$
$F_{t}=12.4 e^{-.291 \times 14.4}$ $\{-12.6 \cos (.071 \times 14.4)$
$+737.2 \sin (.071 \times 14.4)\}$
$=117 \mathrm{kips}$
TYPE II Solution ( $C-8000$ )

$$
\begin{aligned}
F_{t} & =12.4\left\{-202 e^{-.547 \times 14.4}+215 e^{-.217 \times 14.4}\right\} \\
& =116 \text { kips }
\end{aligned}
$$

Interpolating for $C=7100$

$$
F_{t}=116.6 \mathrm{kips}
$$

Step $6 \quad$ Find $F_{S}$
For a side force:

$$
\begin{aligned}
F_{S} & =\frac{1}{2} R \\
& =\frac{1}{2}(40 \text { tons })=20 \text { tons } \\
& =40 \mathrm{kips}
\end{aligned}
$$

Step 7 Find $\mathrm{F}_{\mathrm{d}}$

$$
\begin{aligned}
F_{d} & =2 J_{c} F_{\max }=2(0.1)(908) \\
& =182 \mathrm{kips}
\end{aligned}
$$

Step $8 \quad$ Find $T_{\max }$

| $F_{\max }$ | 908 |
| :--- | :---: |
| $-F_{t}$ | -117 |
| $-F_{s}$ | -40 |
| $-F_{d}$ | -182 |
| $T_{\max }$ | 569 kips |

Step $9 \quad$ Find Maximum Tension Stress
$\sigma_{t}=569 / 305=1.87 \mathrm{ksi}$
occurring at approximately 15.6 feet below the top of the pile.

This stress exceeds the prestress, so a thicker cushion is required. Try nine sheets of $3 / 4$-inch plywood.

Step 1 Driving System Constants
All constants remain the same except $C$.
$C=\frac{400 \times 30}{(9 \times 3 / 4)(0.75)}$
$=2370 \mathrm{k} / \mathrm{in}$

Step 2 Find Force Wave Constants
$\propto=0.122$
$t_{p}=5.9$
$\omega=0.139$
$F / V=56.0$
$A=-12.7$
$B=147.3$

Step $3 \quad$ Find Critical Depth

$$
\begin{aligned}
x_{c} & =11.12(5.9) / 2 \\
& =31.1 \mathrm{ft}
\end{aligned}
$$

Step $4 \quad$ Find $F_{\max }$

$$
\begin{aligned}
F_{\max } & =(56)(12.4) \\
& =694 \mathrm{kips}
\end{aligned}
$$

Step $5 \quad$ Find $F_{t}$

$$
t_{d}=\text { unchanged }=14.4 \mathrm{Msec}
$$

## TYPE I Solution

$$
\begin{aligned}
F_{t}=12.4 e^{-.122 \times 14.4} & \{-12.7 \cos (.139 \times 14.4) \\
& +147.3 \sin (.139 \times 14.4)\}
\end{aligned}
$$

$$
=298 \mathrm{kips}
$$

Step $6 \quad$ Find $F_{S}$
Same as above:

$$
F_{s}=40 \mathrm{kips}
$$

Step $7 \quad$ Find $F_{d}$

$$
\begin{aligned}
F_{d} & =2(0.1)(694) \\
& =138 \mathrm{kips}
\end{aligned}
$$

Step $8 \quad$ Find $T_{\text {max }}$

| $F_{\text {max }}$ | 694 |
| :--- | ---: |
| $-F_{t}$ | -298 |
| $-F_{s}$ | -40 |
| $-F_{d}$ | -138 |
| $T_{\max }$ | 218 |

Step 9 Find Maximum Tension Stress
$\sigma_{t}=218 / 305=0.71 \mathrm{ksi}$
Occurring at approximately 31.1 feet below
the pile top.
The tension stress is less than the prestress, so the cushion is sufficient.

## REFERENCE

Parker, Eric J., "Tension Cracking in Concrete Piles Driven by Air/Steam Hammers", Masters thesis, Department of Civil, Environmental and Architectural Engineering, University of Colorado, 1979.

## APPENDIX

## PILE TABLES

| Constant | Units |
| :---: | :---: |
| $\propto$ | Msec ${ }^{-1}$ |
| $\omega$ | Msec ${ }^{-1}$ |
| A | K-Sec/Ft |
| B | K-Sec/Ft |
| $t_{p}$ | Msec |
| F/V | K-Sec/Ft |
| $S_{1}$ | Msec ${ }^{-1}$ |
| $s_{2}$ | Msec ${ }^{-1}$ |
| P | K-Sec/Ft |
| Q | K-Sec/Ft |



RAM WEIGHT = 3.0 KIPS
PILE SIZE 12 INCH SQUARE
AREA $=144.0$ SQ. 1 N.


RAM WEIGHT $=3.0$ KIPS
PILE SIZE 14 INCH SQUARE
AREA $=196.0$ SQ. IN.


| RAM WEIGHT $=5.0 \mathrm{KIPS}$ |  |  |  |  |  |  |  | $\begin{aligned} & \text { TYPE 1 } \\ & \text { (TYPE 1I) } \end{aligned}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| pile size 10 inch square AREA - 100.0 SQ. IN. |  |  |  |  |  |  |  |  |  |  |  |  |  |
| helmet | CUSHION <br> (H/IN) |  |  | $\begin{gathered} E=4000 . \mathrm{KSI} \\ 1=36.0 \end{gathered}$ |  |  |  | $E=6000 . \mathrm{KSI}$ |  |  |  |  |  |
|  |  | $\begin{aligned} & \text { ALPHA } \\ & (51) \end{aligned}$ | $\begin{aligned} & \text { OMEGA } \\ & (52) \end{aligned}$ | $\begin{gathered} A \\ (P) \end{gathered}$ | $\begin{gathered} 8 \\ (0) \end{gathered}$ | IP | ( $F / V$ ) | $\begin{aligned} & \text { ALPHA } \\ & \text { (SI) } \end{aligned}$ | $\begin{aligned} & \text { OMEGA } \\ & (52) \end{aligned}$ | $\left(\begin{array}{l} \text { ( }) \end{array}\right.$ | $\begin{aligned} & 8 \\ & (Q) \end{aligned}$ | TP | (F/V) |
| $\begin{aligned} & H=.85 \\ & K=20000 . \end{aligned}$ | 250. | . 049 | . 109 | -4.0 | 18.6 | 8.7 | 11.4 | . 045 | . 111 | -4.9 | 18.1 | 8.4 | 11.9 |
|  | 500. | . 045 | . 146 | -4.0 | 28.1 | 6.5 | 14.5 | . 075 | . 152 | -4.9 | 26.9 | 6.3 | 15.5 |
|  | 750. | . 121 | . 168 | -4.0 | 36.8 | 4.9 | 16.6 | . 104 | . 179 | -4.8 | 34.4 | 4.8 | 17.9 |
|  | 1000. | . 157 | . 180 | -3.9 | 45.8 | 4.6 | 17.0 | . 133 | . 198 | -4.8 | 41.5 | 4.6 | 19.5 |
|  | 1500. | . 228 | . 183 | -3.9 | 67.8 | 3.1 | 20.0 | . 191 | . 221 | -4.8 | 56.0 | 3.1 | 22.0 |
|  | 2000. | . 299 | . 156 | -4.0 | 106.0 | 2.9 | 21.5 | . 249 | . 227 | -4.8 | 72.6 | 2.9 | 23.9 |
| $\begin{aligned} & H=.85 \\ & K=30000 . \end{aligned}$ | 250. | . 049 | . 109 | -4.0 | 18.6 | 8.6 | 11.4 | . 045 | . 111 | -4.9 | 18.1 | 8.4 | 11.9 |
|  | 500. | . 085 | .146 | -4.0 | 28.1 | 6.6 | 14.5 | . 075 | . 152 | -4.9 | . 26.9 | 5.9 | 15.5 |
|  | 750. | . 121 | . 168 | -4.0 | 36.8 | 5.3 | 16.5 | . 104 | . 179 | -4.9 | 34.5 | 5.3 | 17.8 |
|  | 1000. | . 157 | .180 | -4.0 | 45.9 | 4.0 | 18.0 | .133 | . 198 | -4.8 | 41.6 | 4.1 | 19.6 |
|  | 1500. | . 229 | . 182 | -4.0 | 68.0 | 3.7 | 19.7 | . 192 | . 221 | -4.8 | 56.1 | 3.8 | 21.9 |
|  | 2000. | . 300 | . 154 | -4.0 | 107.1 | 2.5 | 21.5 | . 250 | . 227 | -4.8 | 72.9 | 2.5 | 23.7 |
| $\begin{aligned} & H=1.00 \\ & K=20000 . \end{aligned}$ | 250. | . 049 | . 108 | -3.9 | 18.4 | 9. 0 | 11.2 | . 045 | . 109 | -4.8 | 17.9 | 8.5 | 11.7 |
|  | 500. | . 085 | . 144 | -3.9 | 27.9 | 5.4 | 14.3 | . 074 | . 150 | -4.7 | 26.7 | 6.4 | 15.2 |
|  | 750. | . 121 | . 165 | -3.9 | 36.6 | 5.1 | 16.3 | . 104 | . 176 | -4.7 | 34.1 | 5.1 | 17.6 |
|  | 1000. | . 157 | . 177 | -3.9 | 45.6 | 4.9 | 17.4 | . 133 | . 195 | -4.7 | 41.2 | 4.9 | 19.1 |
|  | 1500. | . 228 | . 177 | -3.9 | 68.3 | 3.2 | 19.8 | . 191 | .217 | -4.7 | 55.8 | 3.3 | 21.8 |
|  | 2000. | . 299 | . 146 | -3.9 | 110.0 | 3.0 | 21.1 | . 249 | . 221 | -4.7 | 72.8 | 3.0 | 23.5 |
| $\begin{aligned} & H=1.00 \\ & K=30000 . \end{aligned}$ | 250. | . 049 | . 108 | -3.9 | 18.4 | 8.0 | 11.2 | . 045 | . 109 | -4.8 | 17.9 | 8.1 | 11.7 |
|  | 500. | . 085 | . 144 | -3.9 | 27.9 | 6.1 | 14.4 | . 074 | . 150 | -4.8 | 26.7 | 6.3 | 15.3 |
|  | 750. | . 121 | . 165 | -3.9 | 36.6 | 4.3 | 16.2 | . 104 | . 176 | -4.8 | 34.1 | 4.4 | 17.5 |
|  | 1000. | . 157 | . 177 | -3.9 | 45.7 | 4.2 | 17.8 | . 133 | . 195 | -4.7 | 41.3 | 4.3 | 19.3 |
|  | 1500. | . 229 | .177 | -3.9 | 68.5 | 2.6 | 19.5 | . 192 | . 216 | -4.7 | 55.9 | 4.0 | 21.3 |
|  | 2000. | . 300 | . 145 | -3.9 | 111.2 | 2.8 | 21.3 | . 250 | . 221 | -4.7 | 73.1 | 2.6 | 23.5 |














RAM WEIGHT $=10.0$ KIPS
PILE SIIE 22 INCH SQUARE HC AREA $=351.0$ SQ. IN.

| HELMET | CUSHION <br> (K/IN) |  | $\begin{gathered} E=4000 . K S I \\ 1=126.3 \end{gathered}$ |  |  |  |  | $\begin{aligned} E & =6000 . K S I \\ 1 & =154.7 \end{aligned}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { ALPHA } \\ & \text { (S1) } \end{aligned}$ | $\begin{aligned} & \text { OMEGA } \\ & (\mathrm{S} 2) \end{aligned}$ | $\begin{gathered} A \\ (P) \end{gathered}$ | $\begin{gathered} B \\ (Q) \end{gathered}$ | TP | (F/V) | $\begin{aligned} & \text { ALPHA } \\ & (S i) \end{aligned}$ | $\begin{aligned} & \text { OMEGA } \\ & (S 2) \end{aligned}$ | $\stackrel{A}{(P)}$ | $\begin{gathered} 8 \\ (0) \end{gathered}$ | TP | (F/V) |
| $\begin{aligned} & H=2.20 \\ & K=40000 . \end{aligned}$ | 1000. | . 063 | . 153 | -13.4 | 50.3 | 5.8 | 33.1 | . 060 | . 155 |  |  |  |  |
|  | 2000. | .103 | . 210 | $-13.3$ | 74.7 | 4.6 | 42.8 | . 0693 | .155 .215 | -16.4 -16.2 | 49.0 72.5 | 5.6 4.4 | $\begin{aligned} & 34.3 \\ & 45.2 \end{aligned}$ |
|  | 4000. | . 184 | . 274 | -13.1 | 115.2 | 3.2 | 54.4 | . 159 | . 2150 | -16.2 -15.9 | 72.5 108.7 | 4.4 3.2 | $\begin{aligned} & 45.2 \\ & 58.4 \end{aligned}$ |
|  | 6000. | . 264 | . 305 | -12.9 | 155.3 | 2.8 | 60.0 | . 224 | . 336 | -15.9 -15.7 | 108.7 140.8 | 3.2 2.8 | $65.7$ |
|  | 8000. 10000 | . 344 | . 313 | -12.9 | 201.2 | 2.4 | $63.2$ | . 288 | . 365 | - 15.6 | 172.6 | 2.3 | $70.5$ |
|  | 10000. | . 422 | . 301 | -13.0 | 260.7 | 1.4 | 68.0 | . 352 | . 381 | -15.5 | 206.2 | 1.7 | $75.0$ |
| $\begin{aligned} & H=2.20 \\ & K=60000 . \end{aligned}$ | 1000. | . 063 | . 153 | -13.4 | 50.2 | 6.1 | 33.0 | . 060 | . 155 | -16.4 |  |  |  |
|  | 2000. | .104 | . 210 | $-13.3$ | 74.7 | 4.4 | 43.1 | . .060 | .155 .215 | -16.4 -16.3 | 49.0 72.4 | 5.8 4.3 | 34.2 45.4 |
|  | 4000 . | . 185 | . 274 | -13.2 | 115.4 | 2.8 | 54.3 | .093 .160 | . 2290 | -16.3 | 108.8 | 4.3 2.9 | $\begin{aligned} & 45.4 \\ & 58.2 \end{aligned}$ |
|  | 6000. | . 266 | . 305 | $-13.1$ | 155.9 | 2.6 | 61.3 | . 226 | . .336 | -16.0 | 108.8 | 2.9 2.6 | $\begin{aligned} & 58.2 \\ & 66.6 \end{aligned}$ |
|  | $\theta 000 .$ | .347 | . 312 | -13.1 | 202.7 | 2.4 | 64.9 | . 291 | . 365 | -15.9 | 173.4 | 2.4 | 71.7 |
|  | 10000. | . 427 | . 299 | $-13.2$ | 264.4 | 2.2 | 66.9 | . 356 | . 380 | -15.8 | 207.8 | 2.2 | 74.9 |
| $\begin{aligned} & H=2.40 \\ & K=40000 . \end{aligned}$ | 1000. | . 062 | . 152 | -13.2 | 49.9 | 6.0 | 32.8 | . 060 | . 153 |  |  |  |  |
|  | 2000. | .103 | . 208 | -13.1 | 74.2 | 4.6 | 32.8 42.2 | . 0693 | .153 .213 | -16.1 -16.0 | 48.7 72.0 | 5.8 4.3 | 34.0 44.8 |
|  | 4000. | .184 | . 271 | -12.9 | 114.7 | 3.3 | 53.8 | . 159 | . 287 | -15.7 | 108.1 | 3.3 | 44.8 57.8 |
|  | 6000. | . 264 | .301 | -12.8 | 155.1 | 2.8 | 59.1 | . 224 | . 332 | -15.5 | 140.2 | 2.8 | 64.8 |
|  | 8000. | . 344 | . 308 | -12.8 | 201.8 | 1.6 | 62.5 | . 289 | . 360 | -15.4 | 172.2 | 2.3 | 69.4 |
|  | 10000 , | .423 | . 294 | -12.8 | 263.5 | 1.4 | 67.6 | . 353 | . 375 | -15.3 | 206.3 | 1.6 | 79.4 |
| $\begin{aligned} & H=2.40 \\ & K=60000 . \end{aligned}$ | 1000. | . 062 | . 152 | -13.2 | 49.9 | 6.2 | 32.7 | . 060 | . 153 | -16.2 | 48.6 |  |  |
|  | 2000. | . 103 | . 208 | -13.1 | 74.2 | 4.5 | 42.7 | . 093 | . 213 | -16.2 | 48.6 71.9 | 5.9 4.4 | 33.9 44.9 |
|  | 4000. | . 185 | . 271 | $-13.0$ | 114.8 | 2.8 | 53.9 | . 159 | . 287 | -15.9 | 108.1 | 3.4 | 44.9 57.8 |
|  | 6000. | . 266 | . 301 | -13.0 | 155.6 | 2.6 | 60.6 | . 226 | . 332 | -15.8 | 140.5 | 2.7 | 65.9 |
|  | 8000. 10000. | . 347 | .307 | $-13.0$ | 203.1. | 2.5 | 64.0 | . 291 | . 360 | -15.7 | 172.9 | 2.5 | 70.7 |
|  | 10000. | . 427 | . 291 | -13.0 | 267.0 | 2.3 | 65.7 | .357 | . 374 | -15.6 | 207.7 | 2.2 | 73.8 |



| RAM WEIGHT $=15.0 \mathrm{KIPS}$ <br> PILE SIZE 18 InCh SQuare AREA = 324.0 SQ. IN. |  |  |  |  |  |  |  | $\begin{aligned} & \text { TYPE I } \\ & \text { (TYPE II) } \end{aligned}$ |  |  |  | $\text { tP } \quad(F / V)$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| helmet | CUSHION (K/IN) |  |  | $\begin{array}{rl} E & =4000 . \mathrm{KSI} \\ 1 & 116.6 \end{array}$ |  |  | ( $F / V$ ) | $\begin{aligned} & \text { ALPHA } \\ & \text { (S1) } \end{aligned}$ | $\begin{aligned} & \text { OMEGA } \\ & \text { (S2) } \end{aligned}$ | $\begin{aligned} E & =6000 . \mathrm{kSI} \\ I & =142.8 \end{aligned}$ |  |  |  |
|  |  | $\begin{aligned} & \text { ALPHA } \\ & (\mathrm{S} 1) \end{aligned}$ | $\begin{aligned} & \text { DMEGA } \\ & \text { (S2) } \end{aligned}$ | $\hat{(P)}$ | $\begin{gathered} 8 \\ (2) \end{gathered}$ | TP |  |  |  | $\hat{(A)}$ | $\begin{gathered} B \\ (0) \end{gathered}$ |  |  |
| $\begin{aligned} & H=1.70 \\ & K=40000 . \end{aligned}$ | 1000. | . 059 | . 129 | -13.5 | 66.5 | 7.1 | 40.1 | . 054 | .131 | -16.5 | 64.7 | 7.1 |  |
|  | 2000. | . 103 | . 171 | -13.3 | 100.9 | 5.1 | 50.8 | . 090 | . 179 | -16.3 | 94.7 | 5.3 | 42.0 54.5 |
|  | 3000. | . 147 | . 195 | -13.1 | 132.7 | 4.4 | 57.2 | . 125 | . 210 | -16.3 | 96.3 123.3 | 4.4 | 54.5 62.2 |
|  | 4000. | . 190 | . 208 | -13.0 | 166.2 | 3.4 | 62.0 | . 161 | . 231 | -15.9 | 149.1 | 3.4 | 62.2 |
|  | 6000. | . 275 | . 205 | -12.9 | 251.4 | 3.0 | 68.7 | . 230 | . 255 | -15.6 | 202.2 | 3.0 | 76.9 |
|  | 8000. | . 360 | . 163 | -12.9 | 418.3 | 2.6 | 72.3 | . 299 | . 258 | -15.4 | 264.4 | 2.7 | 76.1 81.2 |
| $\begin{aligned} & H=1.70 \\ & K=60000 . \end{aligned}$ | 1000. | . 059 | . 129 | -13.5 | 66.5 | 7.3 | 40.1 | . 054 | . 131 | -16.6 | 64.7 | 7.1 |  |
|  | 2000. | . 103 | . 171 | -13.4 | 100.9 | 5.4 | 50.8 | . 090 | . 179 | -16.4 | 96.3 | 5.3 | 42.0 54.4 |
|  | 3000. | . 147 | . 195 | $-13.3$ | 133.0 | 4.1 | 57.5 | . 126 | . 210 | -16.4 | 96.3 123.5 | 5.3 4.2 | 54.4 62.3 |
|  | 4000. | . 191 | . 208 | -13.2 | 166.9 | 3.8 | 61.9 | . 162 | . 231 | -16.3 | 129.5 | 4.2 | 62.3 67.8 |
|  | 6000. | . 278 | . 204 | -13.2 | 254.5 | 2.8 | 68.5 | . 233 | . 254 | -16.1 | 149.5 | 3.8 2.8 | 67.8 75.9 |
|  | 8000. | . 364 | . 158 | -13.1 | 434.7 | 2.5 | 73.4 | . 303 | . 257 | -16.0 | 268.0 20.0 | 2.8 2.5 | 75.9 81.9 |
| $\begin{aligned} & H=1.80 \\ & K=40000 . \end{aligned}$ | 1000. | . 059 | . 128 | -13.4 | 66.3 | 7.1 | 39.9 | . 054 | . 130 | -16.4 | 64.5 | 7.1 |  |
|  | 2000. | . 103 | . 171 | -13.2 | 100.7 | 5.1 | 50.7 | . 090 | . 178 | -16.4 | 64.5 | 5.3 | 41.9 54.3 |
|  | 3000. | . 147 | . 195 | -13.1 | 132.6 | 4.4 | 56.9 | . 125 | . 209 | -16.0 | 123.1 | 4.4 | 61.9 |
|  | 4000. | . 190 | . 207 | -13.0 | 166.2 | 3.4 | 61.8 | .161 | . 230 | -15.8 | 148.9 | 4.4 | 67.9 |
|  | 6000. | .276 | . 203 | -12.9 | 252.2 | 3.0 | 68.4 | . 230 | . 253 | -15.5 | 202.2 | 3.0 | 75.8 |
|  | 8000. | . 360 | . 160 | -12.9 | 424.1 | 2.7 | 71.8 | . 299 | . 256 | -15.4 | 264.9 | 2.7 | 80.8 |
| $\begin{aligned} & H=1.80 \\ & K=60000 . \end{aligned}$ | 1000. | . 059 | . 128 | -13.4 | 66.3 | 7.3 | 39.9 | . 054 | . 130 |  |  |  |  |
|  | 2000. | . 103 | . 171 | $-13.3$ | 100.7 | 5.4 | 50.5 | .090 | . 178 | -16.5 | 64.5 | 7.1 | 41.9 |
|  | 3000. | . 147 | . 195 | -13.3 | 132.9 | 4.2 | 57.3 | . 126 | . 209 | -16.3 | 96.1 123.3 | 5.3 | 54.2 |
|  | 4000. | . 191 | . 207 | -13.2 | 166.8 | 3.8 | 61.5 | . 162 | . 230 | -16.1 | 123.3 | 4.2 3.8 | 62.0 |
|  | 6000. | . 278 | . 202 | -13.1 | 255.2 | 2.8 | 68.3 | . 233 | . 253 | -15.9 | 203.5 | 3.8 2.8 | 75.5 |
|  | 8000. | . 364 | . 155 | -13.1 | 440.8 | 2.5 | 73.1 | . 303 | . 255 | -15.8 | 268.4 | 2.5 | 81.7 |



RAM WEIGHT $=15.0$ KIPS
TYPE 1
PILE SIZE 22 INCH SQUARE AREA $=4 B 4.0$ SQ. IN.




RAM WEIGHT $=15.0$ KIPS
PILE SIZE 24 INCH SQUARE HC AREA $=399.0$ SQ. IN.


RAM WEIGHT $=20.0 \mathrm{KIPS}$
PILE SIZE 18 INCH SQUARE AREA $=324.0$ SO. 1 N .




## RAM WEIGHT $=20.0$ KIPS

PILE SIZE 24 INCH SQUARE
AREA $=576.0$ SQ. IN.

| HELMET | $\begin{aligned} & \text { CUSHION } \\ & (K / I N) \end{aligned}$ |  | $\begin{array}{ll} E & =4000 . K S 1 \\ 1 & =207.3 \end{array}$ |  |  |  |  | $\begin{aligned} & E=6000 . k S 1 \\ & I=253.9 \end{aligned}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ALPHA <br> (Si) | $\begin{aligned} & \text { OMEGA } \\ & (52) \end{aligned}$ | $\begin{gathered} A \\ (\mathrm{P}) \end{gathered}$ | $\begin{gathered} 8 \\ (Q) \end{gathered}$ | TP | (F/V) | $\begin{aligned} & \text { ALPHA } \\ & \text { (SI) } \end{aligned}$ | $\begin{aligned} & \text { OMEGA } \\ & \text { (S2) } \end{aligned}$ | $\begin{gathered} \mathbf{A} \\ (\mathbf{P}) \end{gathered}$ | $\begin{gathered} B \\ (0) \end{gathered}$ | TP | (F/V) |
|  | 1000. | . 044 | . 115 | -24.0 | 72.7 | 7.8 | 50.8 | . 044 | . 115 | -29.5 | 70.7 | 7.2 | 52.4 |
| $K=40000$ | 2000. | . 064 | . 159 | -23.6 | 107.4 | 5.8 | 67.0 | . 064 | . 161 | -29.0 | 104.8 | 5.7 | 70.1 |
|  | 4000. | . 117 | . 214 | -23.0 | 160.9 | 4.3 | 85.7 | . 103 | . 221 | $-28.1$ | 15A.9 | 4.2 | 91.4 105.0 |
|  | 6000. | . 165 | . 248 | -22.4 | 208.0 | 3.5 | 97.3 | . 142 | . 262 | $-27.3$ | 196.3 | 3.6 | 105.0 |
|  | 8000 . | . 212 | . 269 | -22.0 | 254.3 | 3.1 | 105.3 | . 180 | . 291 | -26.7 | 234.3 270.8 | 3.2 | 114.7 122.2 |
|  | 10000. | . 258 | . 280 | -21.7 | 302.6 | 2.8 | 111.2 | .217 | . 313 | -26.2 | 270.8 | 2.8 | 122.2 |
| $\begin{aligned} & H=2.20 \\ & K=60000 . \end{aligned}$ | 1000. | . 044 | . 115 | -24.1 | 72.7 | 7.5 | 50.7 | . 044 | . 115 | -29.6 | 70.6 | 7.0 | 52.4 |
|  | 2000. | . 069 | . 159 | $-23.9$ | 107.4 | 5.7 | 67.0 | . 064 | . 161 | -29.3 | 104.7 | 5.7 | 70.0 |
|  | 1000. | .118 | .214 | -23.4 | 161.2 | 4.4 | 85.7 | .104 | . 222 | -28. | 155 | 4.2 | 91.3 105.0 |
|  | 6000. | . 167 | . 248 | -23.1 | 209.0 | 3.4 | 97.2 | . 144 | . 262 | -28.1 | 197.1 | 3.5 | 115.1 |
|  | 8000. | . 215 | . 269 | -22.8 | 256.4 | 3.0 | 105. ${ }^{1} 12$ | . 183 | - 292 | -27.7 | 235.9 273.6 | 3.0 | 115.1 122.8 |
|  | 10000. | . 262 | . 280 | -22.5 | 306.7 | 2.7 | 112.1 | .221 | . 314 | -27.3 | 273.6 | 2.7 | 122.8 |
| $H=2.40$$K=40000$. | 1000. | . 044 | .114 | -23.8 | 72.4 | 7.9 | 50.5 | . 044 | . 114 | -29.2 | 70.5 | 7.2 | 52.1 |
|  | 2000. | . 069 | . 158 | -23.5 | 107.0 | 5.8 | 66.7 | . 064 | . 160 | -28.7 | 104.4 | 5.8 | 69.7 90.9 |
|  | 4000. | .117 | . 213 | -22.8 | 160.4 | 4.3 | 85. 3 | . 103 | - 220 | -27.9 | 154.3 | 4.2 | 104.4 |
|  | 6000. | . 165 | . 246 | -22.3 | 207.6 | 3.6 | 96.8 | . 142 | . 260 | -27.1 | 195.8 | 3.6 | 104.4 |
|  | 8000. | . 212 | . 267 | -21.9 | 254.1 | 3.1 | 104.6 | . 180 | . 290 | -26.6 | 233.8 | 2.2 | 114.0 121.4 |
|  | 10000. | . 258 | . 278 | -21.7 | 302. 8 | 2.8 | 110.4 | . 217 | .311 | -26. 1 | 270.4 | 2.8 | 121.4 |
| $\begin{aligned} & H=2.40 \\ & K=60000 . \end{aligned}$ | 1000. | . 044 | . 114 | -23.9 | 72.4 | 7.6 | 5.0 .5 | . 044 | . 114 | -29.3 | 70.4 | 7.0 | 52.1 |
|  | 2000. | . 069 | .158 | -23.7 | 107.0 | 5.8 | 66.6 | . 064 | . 160 | -29.0 | 104.3 | 5.8 | 69.7 |
|  | 4000. | .118 | . 213 | -23.3 | 160.7 | 4.4 | 85.2 | . 104 | . 220 | -2日.5 | 154.5 | 4.2 | 90.8 |
|  | 6000. | . 167 | . 247 | -22.9 | 208.5 | 3.5 | 96.7 | .144 | . 261 | -28.0 | 196.4 | 3.5 | 104.4 |
|  | 8000. | .215 | . 267 | -22.6 | 256.1 | 3.0 | 105.2 | . 183 | . 290 | -27.5 | 235.3 | 3.1 | 114.5 |
|  | . 1000 | . 263 | . 278 | -22.4 | 306.7 | 2.7 | 111.3 | .221 | . 312 | -27.2 | 273.1 | 2.8 | 122.1 |



| RAM WEIGHT $=20.0 \mathrm{KIPS}$ <br> PILE SIZE 22 INCH SQUARE HC AREA = 351.0 SQ. IN. |  |  |  |  |  |  |  | $\begin{gathered} \text { TYPE I } \\ \text { (TYPE II) } \end{gathered}$ |  |  |  |  | ( $F / V$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |
| helmet | CUSHION <br> (K/IN) |  |  | $\begin{aligned} E & =4000 . K S I \\ I & =126.3 \end{aligned}$ |  |  |  |  |  |  |  | $\begin{gathered} E=6000 . K S 1 \\ 1=154.7 \end{gathered}$ |  |  |  |  |
|  |  | $\begin{aligned} & \text { ALPHA } \\ & \text { (S1) } \end{aligned}$ | $\begin{aligned} & \text { OMEGA } \\ & (\$ 2) \end{aligned}$ | $\begin{gathered} A \\ (P) \end{gathered}$ | $\begin{gathered} B \\ (0) \end{gathered}$ | TP | (F/V) | $\begin{aligned} & \text { ALPHA } \\ & \text { (S1) } \end{aligned}$ | $\begin{aligned} & \text { OMEGA } \\ & (\mathrm{S} 2) \end{aligned}$ | $\stackrel{A}{(p)}$ | $\begin{gathered} 8 \\ (0) \end{gathered}$ | TP |  |
| $\begin{aligned} & H=2.20 \\ & K=40000 . \end{aligned}$ | 1000. | . 053 | . 111 | -14.6 | 77.7 | 8.4 | 45.6 | . 048 | . 113 | -17.9 | 75.4 | 8.0 |  | 48.0 |
|  | 2000. | . 093 | .146 | -14.4 | 118.9 | 5.9 | 57.4 | . 081 | . 153 | -17.7 | 112.7 | 6.1 | 61.7 |
|  | 4000. | . 174 | . 171 | -14.2 | 202.1 | 3.8 | 69.5 | . 146 | . 195 | -17.3 | 177.1 | 4.1 | 76.4 |
|  | 6000. | . 253 | . 157 | -14.1 | 328.4 | 3.4 | 76.8 | . 211 | . 210 | -17.0 | 245.6 | 3.5 | 85.3 |
|  | 8000. | . 330 | . 090 | -14.1 | 761.4 | 3.1 | 80.4 | . 274 | . 205 | -16.8 | 333.3 | 3.1 | 90.8 |
|  | 10000. | (.549) | (.265) | (-292.) | (307.) | 2.7 | 82.6 | . 336 | . 180 | -16.8 | 471.9 | 2.8 | 94.4 |
| $\begin{aligned} & H=2.20 \\ & K=60000 . \end{aligned}$ | 1000. | . 053 | . 111 | -14.7 | 77.7 | 8.4 | 45.6 | . 048 | . 113 | -18.0 | 75.4 | 8.3 | 48.0 |
|  | 2000. | . 094 | . 146 | -14.6 | 119.0 | 6.1 | 57.3 | . 081 | . 153 | -17.8 | 112.8 | 6.1 | 61.7 |
|  | 4000. | . 175 | . 171 | -14.4 | 203.1 | 4.4 | 69.4 | . 147 | . 195 | -17.6 | 177.7 | 4.3 | 76.4 |
|  | 6000. | . 255 | . 156 | -14.3 | 333.8 | 3.0 | 76.8 | . 213 | . 210 | -17.4 | 247.5 | 3.1 | 85.1 |
|  | 8000. | . 335 | . 082 | -14.4 | 847.1 | 2.7 | 81.8 | . 277 | . 204 | -17.3 | 338.9 | 2.8 | 91.6 |
|  | 10000. | (.565) | (.261) | (-275.) | (289.) | 2.6 | 84.6 | . 341 | . 175 | -17.2 | 490.0 | 2.7 | 95.9 |
| $\begin{aligned} & H=2.40 \\ & K=40000 . \end{aligned}$ | 1000. | . 053 | . 110 | -14.5 | 77.4 | 0.5 | 45.3 | . 048 | . 113 | -17.8 | 75.1 | 8.1 | 47.7 |
|  | 2000. | . 093 | . 145 | -14.3 | 118.5 | 6.0 | 57.1 | . 081 | . 152 | -17.5 | 112.3 | 6.1 | 61.4 |
|  | 4000. | . 174 | . 170 | -14.1 | 202.2 | 3.8 | 69.3 | . 146 | . 194 | -17.1 | 176.8 | 4.1 | 76.0 |
|  | 6000. | . 253 | . 155 | -14.0 | 331.1 | 3.4 | 76.3 | . 211 | . 209 | -16.9 | 245.7 | 3.5 | 84.9 |
|  | 8000. | . 331 | . 083 | -14.1 | 815.8 | 3.1 | 79.7 | . 274 | . 203 | -16.8 | 334.9 | 3.1 | 90.0 |
|  | 10000. | (.555) | (.260) | (-279.) | (293.) | 2.7 | 81.6 | . 336 | . 176 | -16.8 | 478.9 | 2.8 | 93.4 |
| $\begin{aligned} & H=2.40 \\ & K=60000 . \end{aligned}$ | 1000. | . 053 | .110 | -14.6 | 77.4 | 8.5 | 45.3 | . 048 | .113 | -17.9 | 75.1 | 8.3 | 47.7 |
|  | 2000. | . 094 | .145 | -14.5 | 118.6 | 6.0 | 56.9 | . 081 | . 152 | -17.7 | 112.4 | 6.1 | 61.3 |
|  | 4000. | . 175 | . 170 | -14.3 | 203.1 | 4.4 | 68.8 | . 147 | . 194 | -17.4 | 177.3 | 4.4 | 75.8 |
|  | 6000. | . 255 | . 153 | -14.3 | 336.4 | 3.0 | 76.6 | . 213 | . 208 | -17.3 | 247.6 | 3.1 | 84.8 |
|  | 8000. | . 335 | . 074 | $-14.3$ | 920.2 | 2.8 | 81.3 | . 278 | . 201 | -17.2 | 340.4 | 2.8 | 91.1 |
|  | . 10000. | (.571) | (.256) | (-264.) | (278.) | 2.7 | 83.8 | . 342 | . 172 | -17.2 | 497.1 | 2.7 | 95.1 |




RAM WEIGHT $=30.0$ KIPS
PILE SIZE 20 INCH SQUARE
AREA $=400.0$ SQ. IN.

| HELMET | $\begin{gathered} \text { CUSHIDN } \\ (K / I N) \end{gathered}$ |  | $\begin{aligned} E & =4000 . K S 1 \\ 1 & =144.0 \end{aligned}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ALPHA (S1) | $\begin{aligned} & \text { OMEGA } \\ & \text { (S2) } \end{aligned}$ | $\begin{gathered} A \\ (P) \end{gathered}$ | $\begin{gathered} 8 \\ (0) \end{gathered}$ | TP | ( $F / V$ ) |
| $\begin{aligned} & H=2.20 \\ & K=40000 . \end{aligned}$ | 1000. | . 045 | . 091 | -17.2 | 57.6 | 10.3 | 55.8 |
|  | 2000. | . 081 | .119 | -16.9 | 150.8 | 7.3 | 69.8 |
|  | 4000. | .151 | . 135 | -16.5 | 265.4 | 5.0 | 83.8 |
|  | 6000. | . 220 | . 112 | -16.3 | 475.8 | 3.8 | 92.0 |
|  | 8000. | (.334) | (.241) | (-751.) | (768.) | 3.5 | 97.1 |
|  | 10000. | (.512) | (.194) | (-266.) | (282.) | 3.1 | 100.4 |
| $\begin{aligned} & H=2.20 \\ & K=60000 . \end{aligned}$ | 1000. | . 045 | . 091 | $-17.3$ | 97.7 | 10.3 | 55.8 |
|  | 2000. | . 081 | .119 | -17.1 | 151.0 | 7.3 | 69.8 |
|  | 4000. | . 152 | . 134 | -16.9 | 267.2 | 4.9 | 84. 1 |
|  | 6000. | . 222 | .110 | -16.7 | 488.6 | 4.0 | 91.4 |
|  | 8000. | (.351) | (.232) | (-594.) | (611.) | 3.0 | 97.5 |
|  | 10000 . | (.528) | (.192) | (-255.) | (272.) | 2.8 | 101.7 |
| $\begin{aligned} & H=2.40 \\ & K=40000 . \end{aligned}$ | 1000. | . 045 | . 091 | -17.1 | 97.4 | 10.3 | 55.6 |
|  | 2000. | . 031 | . 118 | -16.8 | 150.6 | 7.3 | 69.5 |
|  | 4000. | . 151 | . 134 | -16.5 | 265.5 | 5.1 | 83.3 |
|  | 6000. | . 220 | . 110 | -16.3 | 480.6 | 3.8 | 91.7 |
|  | 8000. | (.340) | (.235) | (-663.) | (680.) | 3.5 | 96.7 |
|  | 10000. | (.516) | (.192) | $(-260$. | (276.) | 3.3 | 99.6 |
| $\begin{aligned} & H=2.40 \\ & K=60000 . \end{aligned}$ | 1000. | . 045 | .091 | -17.2 | 97.4 | 10.3 | 55.6 |
|  | 2000. | . 081 | .118 | -17.0 | 150.8 | 7.1 | 69.6 |
|  | 4000. | .152 | .134 | -16.8 | 267.4 | 4.9 | 83.7 |
|  | 6000. | . 222 | . 108 | -16.6 | 493.6 | 3.5 | 90.9 |
|  | $8000 .$ | (.355) | (.228) | (-549.) | (566.) | 3.1 | 97.3 |
|  | 10000 . | (.530) | (.190) | (-250.) | (267.) | 2.9 | 101.3 |

TYPE 1
(TYPE II)
$E=6000 . K S$
$I=176.3$

| ALPHA | OMEGA |
| :--- | :--- |
| $(S 1)$ | $(S 2)$ |
|  |  |
| .041 | .093 |
| .070 | .126 |
| .127 | .158 |
| .183 | .166 |
| .238 | .154 |
| .291 | .120 |
| .041 | .093 |
| .070 | .126 |
| .128 | .158 |
| .185 | .165 |
| .241 | .152 |
| .297 | .114 |
|  |  |
| .041 | .093 |
| .070 | .125 |
| .127 | .157 |
| .183 | .164 |
| .238 | .153 |
| .292 | .117 |
| .041 | .093 |
| .070 | .125 |
| .128 | .157 |
| .185 | .164 |
| .241 | .151 |
| .297 | .111 |

?

| $\stackrel{A}{(P)}$ | $\begin{gathered} B \\ (0) \end{gathered}$ | TP | (F/V) |
| :---: | :---: | :---: | :---: |
| -21.1 | 94.6 | 9.8 | 58.9 |
| -20.7 | 142.0 | 7.3 | 75.4 |
| -20.1 | 226.4 | 5.1 | 92.7 |
| -19.7 | 321.6 | 4.0 | 102.日 |
| -1.9.4 | 456.4 | 3.7 | 109.3 |
| -19.3 | 725.5 | 3.3 | 114.3 |
| -21.2 | 94.6 | 9.7 | 58.9 |
| -21.0 | 142.2 | 7.3 | 75.4 |
| -20.5 | 227.4 | 5.1 | 92.8 |
| -20.3 | 325.0 | 4.1 | 102.6 |
| -20.0 | 467.8 | 3.3 | 109.7 |
| $-19.9$ | 778.6 | 2.9 | 115.2 |
| -20.9 | 94.4 | 9.8 | 50.7 |
| -20.6 | 141.7 | 7.3 | 75.1 |
| -20.0 | 226.2 | 5.1 | 92.3 |
| -19.7 | 322.0 | 4.0 | 102.4 |
| -19.4 | $459.0^{\circ}$ | 3.8 | 108.8 |
| -19.3 | 739.7 | 3.3 | 113.7 |
| -21.1 | 94.4 | 9.8 | 58.7 |
| -20.8 | 141.9 | 7.3 | 75.1 |
| -20.5 | 227.1 | 5.1 | 92.4 |
| -20.2 | 325.3 | 4.1 | 102.1 |
| $-20.0$ | 470.3 | 3.3 | 109.3 |
| -19.9 | 795.1 | 2.9 | 114.8 |

RAM WEIGHT $=30.0$ KIPS
PILE SIZE 22 INCH SQUARE
AREA $=484.0$ SQ. IN.

| HELMET |  | $\begin{aligned} & \text { CUSHION } \\ & (K / I N) \end{aligned}$ |  | $\begin{gathered} E=4000 . K S I \\ I=174.2 \end{gathered}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \text { ALPHA } \\ & \text { (S1) } \end{aligned}$ | $\begin{aligned} & \text { OMEGA } \\ & \text { (S2) } \end{aligned}$ | $\begin{gathered} A \\ (P) \end{gathered}$ | $\begin{gathered} 8 \\ (0) \end{gathered}$ | TP | $(F / V)$ |
|  | $=2.20$ | 1000. | .041 | . 093 | -20.日 | 94.8 | 9.8 | 58.8 |
|  | $=40000$ | 2000. | . 070 | . 125 | -20.5 | 142.4 | 7.3 | 75.1 |
|  |  | 4000. | .128 | . 157 | -19.9 | 227.9 | 5.1 | 92.2 |
|  |  | 6000. | . 185 | .163 | -19.5 | 326.0 | 4.0 | 102.1 |
|  |  | 8000. | .240 | .150 | -19.2 | 469.1 | 3.5 | 108.9 |
|  |  | 10000. | . 295 | .112 | -19.1 | 779.9 | 3.0 | 113.5 |
| $\begin{aligned} & =2.20 \\ & =60000 . \end{aligned}$ |  | 1000. | . 041 | . 093 | -20.9 | 94.8 | 9.8 | 58.8 |
|  |  | 2000. | . 071 | . 126 | -20.7 | 142.6 | 7.3 | 75.1 |
|  |  | 4000. | . 129 | . 157 | -20.3 | 228.9 | 5.0 | 92.3 |
|  |  | 6000. | .167 | .163 | $-20.0$ | 329.6 | 4.1 | 101.9 |
|  |  | 8000. | . 244 | .148 | $-19.8$ | 481.6 | 3.3 | 108.9 |
|  |  | 10000. | .300 | .104 | $-19.7$ | 847.5 | 3.1 | 114.2 |
| $\begin{aligned} & H=2.40 \\ & K=40000 . \end{aligned}$ |  | 1000. | . 041 | . 093 | -20.7 | 94.5 | 9.8 | 58.5 |
|  |  | 2000. | . 070 | . 125 | -20.4 | 142.1 | 7.3 | 58.5 74.8 |
|  |  | 4000. | .128 | . 156 | $-19.8$ | 227.7 | 5.2 | 91.8 |
|  |  | 6000. | . 185 | . 162 | -19.4 | 326.4 | 4.0 | 101.8 |
|  |  | 8000. | . 241 | . 148 | $-19.2$ | 472.1 | 3.6 | $108.4$ |
|  |  | 10000. | . 295 | . 109 | -19.1 | 798.5 | 3.1 | $112.9$ |
| $\begin{aligned} & H \\ & K \end{aligned}$ | $=2.40$ | 1000. | . 041 | .093 | -20.8 | 94.5 | 9.8 |  |
|  | $60000$ | 2000. | . 071 | .125 | -20.6 | 142.3 | 9.8 7.3 | 58.5 74.8 |
|  |  | 4000. | . 129 | . 156 | -20.2 | 228.7 | 5.1 | 91.9 |
|  |  | 6000. | . 187 | . 162 | -20.0 | 329.9 | 4.1 | 101.4 |
|  |  | 8000. 10000. | $.244$ | .146 .101 | -19.8 -19.7 | 484.5 | 3.3 | $108.7$ |
|  |  | 10000. | . 301 | .101 | $-19.7$ | 869.9 | 3.1 | 113.7 |

TYPE 1
(TYPE 11)

RAM WEIGHT $=30.0$ KIPS
TYPEI
(TYPE II)
PILE SIZE 24 INCH SQUARE AREA $=576.0$ SQ. IN.

| helmet |  | $\begin{aligned} & \text { CUSHION } \\ & (K / I N) \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \text { ALPHA } \\ & (S 1) \end{aligned}$ | $\begin{aligned} & \text { OMEGA } \\ & \text { (S2) } \end{aligned}$ |
|  | . 2.20 | 1000. | . 038 | . 094 |
| K | - 40000 . | 2000. | . 063 | . 129 |
|  |  | 4000. | . 111 | .169 |
|  |  | 6000. | .159 | . 189 |
|  |  | 8000. | . 205 | .195 |
|  |  | 10000. | . 251 | .191 |
|  | . 2.20 | 1000. | . 038 | . 094 |
|  | -60000. | 2000. | . 063 | .129 |
|  |  | 4000. | . 112 | .169 |
|  |  | 6000. | .161 | .189 |
|  |  | 8000. | . 209 | . 195 |
|  |  | 10000. | . 256 | .189 |
|  | . 2.40 | 1000. | . 038 | . 094 |
|  | - 40000 . | 2000. | . 063 | . 129 |
|  |  | 4000. | .111 | . 168 |
|  |  | 6000. | . 159 | .188 |
|  |  | 8000. | . 205 | .194 |
|  |  | 10000. | . 251 | .189 |
| $H$$H$ | . 2.40 | 1000. | . 038 | . 094 |
|  | -60000. | 2000. | . 063 | . 129 |
|  |  | 4000. | . 112 | . 168 |
|  |  | 6000. | .161 | .188 |
|  |  | 8000. | . 209 | .193 |
|  |  | 10000. | . 256 | .187 |

$I=207.3$

| $\begin{gathered} A \\ (P) \end{gathered}$ | $\begin{gathered} B \\ (0) \end{gathered}$ | TP | ( F/V) |
| :---: | :---: | :---: | :---: |
| -24.8 | 92.7 | 9.8 | 61.1 |
| -24.3 | 137.5 | 7.2 | 79.4 |
| -23.6 | 210.9 | 5.1 | 99.4 |
| -23.0 | 281.9 | 4.2 | 1.11 .4 |
| -22.6 | 360.5 | 3.6 | 119.7 |
| -22.3 | 457.1 | 3.2 | 125.7 |
| -24.9 | 92.7 | 9.8 | 61.1 |
| -24.6 | 137.6 | 7.2 | 79.4 |
| -24.1 | 211.6 | 5.1 | 99.5 |
| -23.7 | 284.0 | 4.2 | 111.4 |
| -23.4 | 365.6 | 3.5 | 119.7 |
| -23.1 | 468.8 | 3.0 | 126.2 |
| -24.6 | 92.4 | 9.8 | 60.9 |
| -24.2 | 137.2 | 7.3 | 79.1 |
| -23.5 | 210.5 | 5.2 | 99.0 |
| -22.9 | 281.7 | 4.2 | 110.9 |
| -22.5 | 360.9 | 3.6 | 119.2 |
| -22.3 | 458.9 | 3.3 | 125.1 |
| -24.8 | 92.4 | 9.8 | 60.9 |
| -24.5 | 137.3 | 7.3 | 79.1 |
| -24.0 | 211.2 | 5.2 | 99.1 |
| -23.6 | 283.8 | 4.2 | 110.8 |
| -23.3 | 365.9 | 3.5 | 119.3 |
| -23.1 | 470.4 | 3.0 | 125.8 |

$\begin{aligned} E & =6000 . \mathrm{MSI} \\ I & =253.9\end{aligned}$

| RAM WEIGHT $=30.0 \mathrm{KIPS}$ |  |  |  |  |  |  |  | $\begin{aligned} & \text { TYPE I } \\ & \text { (TYPE II) } \end{aligned}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HELMET | CUSHION ( $\mathrm{H} / \mathrm{IN}$ ) |  |  | $\begin{aligned} & E=4000 . \mathrm{KSI} \\ & \mathrm{I}=109 . \mathrm{B} \end{aligned}$ |  |  |  | $\begin{aligned} & E=6000 . \mathrm{KSI} \\ & \mathrm{I} .134 .4 \end{aligned}$ |  |  |  |  |  |
|  |  | $\begin{aligned} & \text { ALPHA } \\ & (S 1) \end{aligned}$ | $\begin{aligned} & \text { DMEGA } \\ & \text { (S2) } \end{aligned}$ | $\begin{aligned} & A \\ & (P) \end{aligned}$ | $\begin{gathered} B \\ (Q) \end{gathered}$ | TP | (F/V) | $\begin{aligned} & \text { ALPHA } \\ & (51) \end{aligned}$ | $\begin{aligned} & \text { OMEGA } \\ & (\mathrm{S} 2) \end{aligned}$ | $\hat{(\hat{P})}$ | $\begin{gathered} B \\ \left(\begin{array}{l} 0 \end{array}\right) \end{gathered}$ | TP | ( $F / V$ ) |
| $\begin{aligned} & H=2.20 \\ & K=40000 . \end{aligned}$ | 1000. | . 054 | . 086 | -13.1 | 104.1 | 10.4 | 50.9 | . 047 | . 090 | -16.1 | 98.9 | 10.3 | 54.7 |
|  | 2000. | . 101 | . 102 | -12.9 | 175.9 | 7.1 | 61.6 | . 085 | . 116 | $-15.8$ | 155.1 | 7.2 | 67.8 |
|  | 4000. | . 193 | . 060 | -12.8 | 597.2 | 4.7 | 71.5 | .161 | . 123 | -15.5 | 290.2 | 5.1 | 80.7 |
|  | 6000. | (.424) | (.144) | (-183.) | (196.) | 3.5 | 78.1 | . 234 | . 077 | -15.3 | 688.7 | 3.7 | 88.4 |
|  | 8000. | (.614) | (.131) | (-139.) | (152.) | 3.3 | 81.1 | (.614) | (.131) | (-139.) | (152.) | 3.3 | 81.1 |
|  | 10000. | (.125) | (.766) | ( 137.) | (-7.) | 3.1 | 82.5 | (.125) | (.766) | ( 137.) | (-7.) | 3.1 | 82.5 |
| $\begin{aligned} & H=2.20 \\ & K=6000 . \end{aligned}$ | 1000. | . 052 | . 086 | -11.9 | 102.7 | 10.8 | 50.8 | . 045 | . 090 | -14.6 | 97.9 | 10.4 | 54.5 |
|  | 2000. | . 094 | .103 | -11.3 | 166.6 | 7.4 | 61.1 | . 079 | . 114 | -13.7 | 148.8 | 7.6 | 67.1 |
|  | 4000. | . 167 | . 086 | -12.3 | 359.9 | 5.0 | 70.2 | . 138 | . 127 | -15.4 | 243.6 | 5.3 | 78.6 |
|  | 6000. | (.278) | (.173) | (-389.) | (404.) | 3.9 | 74.7 | . 185 | . 114 | -20.4 | 355.8 | 4.3 | 84.2 |
|  | 8000. | (.397) | $(.146)$ | (-190.) | (206.) | 3.3 | 77.2 | . 220 | . 087 | -26.5 | 537.0 | 3.6 | 87.5 |
|  | 10000. | (.480) | (.137) | (-155.) | (172.) | 3.1 | 78.7 | . 246 | . 043 | -32.0 | 1186.1 | 3.2 | 89.6 |
| $\begin{aligned} & H=2.40 \\ & K=40000 . \end{aligned}$ | 1000. | . 054 | . 086 | -13.1 | 103.9 | 10.5 | 50.7 | . 047 | . 090 | -16.0 | 98.7 |  |  |
|  | 2000. | . 101 | . 102 | -12.9 | 175.9 | 6.9 | 61.4 | . 085 | . 115 | -15.0 | 98.7 154.9 | 10.4 7.2 | 54.4 67.5 |
|  | 4000. | . 193 | . 058 | -12.8 | 616.3 | 4.0 | 71.4 | . 161 | . 122 | -15.4 | 290.9 | 5.1 | 80. 2 |
|  | 6000. | (.426) | (.142) | (-180.) | (193.) | 3.4 | 77.6 | . 234 | . 075 |  |  |  |  |
|  | 8000. | (.616) | $(.130)$ | (-137.) | (150.) | 3.3 | 80.6 | (.616) | $\left(\begin{array}{l}\text { ( } \\ (130)\end{array}\right.$ | (-157.) | (150.) | 3.8 3.3 | 88.1 80.6 |
|  | . 10000. | (.124) | (.706) | ( 135.) | (-7.) | 3.2 | 81.7 | (.124) | (.706) | (135.) | ( -7.$)$ | 3.2 | 81.7 |
| $\begin{aligned} & H=2.40 \\ & H=60000 . \end{aligned}$ | 1000. | . 054 | . 086 | -13.1 | 104.0 |  |  | . 047 |  |  |  |  |  |
|  | 2000. | . 101 | . 102 | -13.0 | 176.3 | 6.8 | 61.5 | . 086 | . 115 | -16.1 | 98.7 155.1 | 10.4 7.1 | 54.4 67.6 |
|  | 4000. | .195 $(432)$ | . 055 | $(-12.9$ | 645.0 | 4.8 | 71.9 | . 162 | . 122 | -15.7 | 293.3 | 4.6 | 80.5 |
|  | 6000. | (.432) | $(.141)$ $(.129)$ | $(-177$. | (190.) | 3.1 | 77.6 | . 237 | (.071 | -15.6 | 754.8 | 3.3 | 87.4 |
|  | . 10000. | (.124) | (.699) | (-136.) | $\left(\begin{array}{l}149 .) \\ (-7 .)\end{array}\right.$ | 3.0 | 81.9 | (.627) | (.129) | $(-136$. | (149.) | 3.0 | 81.9 |
|  | .rooos. | (.124) | (.699) | (134.) | (-7.) | 2.9 | 84.0 | (.124) | (.699) | ( 134.) | (-7.) | 2.9 | 84.0 |

RAM WEIGHT $=30.0 \mathrm{KIPS}$
PILE SIZE 22 INCH SQUARE HC AREA $=351.0$ SQ. IN.

| HElmet |  | CUSHION <br> (K/IN) |  | $\begin{aligned} E & =4000 . \text { KSI } \\ I & =126.3 \end{aligned}$ |  |  |  |  | $\begin{aligned} E & =6000 . K S I \\ & =154.7 \end{aligned}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \text { ALPHA } \\ & \text { (Sit) } \end{aligned}$ | $\begin{aligned} & \text { OMEGA } \\ & (52) \end{aligned}$ | $\begin{gathered} A \\ (P) \end{gathered}$ | $\begin{gathered} \mathbf{B} \\ (0) \end{gathered}$ | TP | $(F / V)$ | $\begin{aligned} & \text { ALPHA } \\ & \text { (S } 1 \text { ) } \end{aligned}$ | $\begin{aligned} & \text { OMEGA } \\ & \text { (S2) } \end{aligned}$ | $\hat{(\hat{P})}$ | $\begin{gathered} B \\ (0) \end{gathered}$ | TP | (F/V) |
|  | -2.20 | 1000. | . 049 | . 089 | -15.1 | 100.3 | 10.2 |  |  |  |  |  |  |  |
| $K$ | - 40000. | 2000. | .090 | .112 | -14.9 | 159.9 | 10.2 7.2 | 53.5 66.0 | .043 .077 | .092 .122 | -18.5 | 96.4 | 10.1 | 57.0 |
|  |  | 4000. | $\begin{array}{r}.170 \\ \hline 170\end{array}$ | . 110 | $-14.6$ | 325.0 | 7.2 5.2 | 66.0 77.8 | .077 .142 | .122 .144 | -18.2 -17.7 | 147.1 247.5 | 7.3 | $71.9$ |
|  |  | 6000. | (.277) | (.220) | (-925.) | (939.) | 3.9 | 84.9 | .142 .206 | . 144 | -17.7 -1.7 .4 | 247.5 | 5.1 | 87.0 |
|  |  | 0000. | (.485) | $(.166)$ | (-213.) | (228.) | 3.4 | 89.3 | . 268 | .136 .091 | -17 | 391.3 | 3.9 | 95.8 |
|  |  | 10000. | (.648) | (.154) | (-169.) | (184.) | 3.1 | 91.6 | (.648) | (.154) | $(-17.3)$ | 772.6 $(184$. | 3.5 3.1 | 101.6 91.6 |
| $\begin{aligned} & H=2.20 \\ & K=6000 . \end{aligned}$ |  | 1000. | . 047 | . 089 | -13.7 | 99.1 | 10.6 |  |  |  |  |  |  |  |
|  |  | 2000. | . 083 | .111 | -12.9 | 153.0 | 10.6 7.7 | 53.5 65.3 | . 041 | .092 .120 | -16.7 | 95.6 | 10.3 | 56.9 |
|  |  | 4000. | .146 | .117 | -14.4 | 263.3 | 7.7 5.3 | 76.0 | . 071 | 120 .142 | -15.7 | 141.8 | 7.6 | 71.0 |
|  |  | 6000. | .196 | . 095 | $-18.5$ | 431.9 | 5.3 4.2 | 76.0 81.3 | 122 .163 | . 142 | -17.9 | 216.5 | 5.4 | 84.3 |
|  |  | 8000. | . 234 | . 042 | -23.3 | 1127.4 | 3.5 | 84.3 | . 163 | .143 .134 | -25.0 | 282.0 | 4.5 | 91.0 |
|  |  | 10000. | (.338) | (.187) | (-332.) | (359.) | 3.2 | 86.2 | . 219 | .134 .121 | -33.9 | 343.6 406.1 | 3.8 | 95.0 |
| $\begin{aligned} & H=2.40 \\ & K=40000 . \end{aligned}$ |  | 1000. | . 049 | . 089 |  |  |  |  |  |  |  |  | 3.3 | 97.7 |
|  |  | 2000. | . 090 | . 1112 | -15.0 -14.8 | 100.0 159.7 | 10.3 | 53.3 | . 043 | . 092 | $-18.4$ | 96.2 | 10.2 | 56.8 |
|  |  | 4000. | . 170 | . 109 | -14.8 | 159.7 326.5 | 7.2 | 65.7 77.4 | . 077 | . 121 | $-18.1$ | 146.9 | 7.4 | 71.6 |
|  |  | 6000. | (.284) | (.213) | (-749.) | (763.) | 4.8 3.9 | 77.4 84.7 | .142 .206 | . 144 | -17.7 | 247.5 | 5.1 | 86.6 |
|  |  | 8000. | (.487) | (.164) | (-209.) | (224.) | 3.9 3.4 | 84.7 88.9 | .206 .269 | .135 .008 | -17.4 | $393.1{ }^{\circ}$ | 3.9 | 95.5 |
|  |  | 10000. | (.651) | (.152) | (-167.) | (181.) | 3.4 | 88.9 90.8 | (.65i) | $(.008)$ | $\left(\begin{array}{c}-17.3 \\ (-167 .)\end{array}\right.$ | 795.1 181 | 3.6 | 101.1 |
| $\begin{aligned} & H=2.40 \\ & K=60000 . \end{aligned}$ |  | 1000. | . 049 | . 089 | -15.1 |  |  |  |  |  |  | (181.) | 3.2 | 90.8 |
|  |  | 2000. | . 090 | . 112 | -15.1 -14.9 | 100.1 160.0 | 10.3 | 53.3 | . 044 | . 092 | $-18.5$ | 96.2 | 10.2 | 56.8 |
|  |  | 4000. | .171 | . 108 | -14.8 | 160.0 330.1 | 7.1 4.9 | 65.8 78.0 | . 077 | . 121 | $-18.3$ | 147.0 | 7.4 | 71.6 |
|  |  | 6000. | (.295) | (.207) | (-598.) | (613.) | 4.9 | 78.0 84.2 | .143 .208 | . 143 | $-18.0$ | 248.8 | 4.8 | 86.8 |
|  |  | 8000. | (.498) | (.163) | (-204.) | (219.) | 3.4 | 84.2 89.8 | .208 .272 | .133 .082 | $-17.8$ | 399.9 | 4.0 | 94.8 |
|  |  | 10000. | (.665) | (.151) | (-164.) | (179.) | 2.8 | 92.8 | (.665) | .082 $(.151)$ | $\begin{gathered} -17.7 \\ (-164 .) \end{gathered}$ | 863.7 | 3.1 | 101.6 |
|  |  |  |  |  |  |  |  |  | (.665) | . 151 ) | (-164.) | (179.) | 2.8 | 92.8 |



